

September 19, 2011

Mr. Randy Benoit
Manager of WPS HQ Project
Winnipeg Police Services
210-266 Graham Avenue
Winnipeg, Manitoba

Dear Sir,

Project No: 60162215 (409.19)

**Regarding: Winnipeg Police Service Firearm Training Facility
Geotechnical Report**

1. Introduction

AECOM Canada Ltd. (AECOM) has been retained by Winnipeg Police Services (WPS) to provide engineering services for the design of an outdoor firing range and associated facilities, including a single storey building, range-master tower, two storm water retention ponds, access road, parking area and earthen berm enclosure for the firing range.

This report summarizes the findings of a geotechnical investigation undertaken at the site and provides geotechnical recommendations related to the design and construction of the proposed facilities.

2. Geotechnical Investigation

The proposed site is located north of Wyper Road, and west of the Trans Canada Highway (Perimeter Highway) in Winnipeg. The property is currently utilized as cropland. The proposed site layout is shown on Figure 01 attached.

Twenty-five test holes were drilled at the proposed site between August 3-4, 2011. The approximate locations are shown on the attached test hole location plan, Figure 01.

The locations of the test holes were originally selected based on a preliminary site plan. The configuration and location of the building and other major structures were changed as the plans developed. Therefore the test holes that were drilled are no longer aligned with the proposed facilities. Due to the accelerated project schedule, and limited budget, it was determined by the project team that performing an additional investigation at the new building location would impact the project delivery schedule and therefore no additional investigation was completed for the new layout. Subsurface conditions in Winnipeg area are reasonably uniform and no major variations are

expected, however the project construction budget and schedule should allow for provisions in the event that adverse groundwater and/or subsurface conditions are encountered.

Detailed logs have been prepared for each test hole to record the description and relative position of the soil strata, the location of the samples, field and laboratory test results, drilling conditions, standpipe installation details and other pertinent information. The test hole logs are attached.

2.1 Subsurface Conditions

In descending order, the general soil profile is as follows,

- Topsoil
- Clay
- Silt Till

Topsoil

A relatively thin layer of topsoil was encountered at all test hole locations, up to 0.3 m thick.

Clay

Clay was encountered at all test hole location to a depth of 8.1 to 8.8 m below grade at the test hole locations. Generally, the clay is silty, moist, stiff, becoming soft with depth, and of high plasticity.

Till

Silt matrix till was encountered beneath the clay. The depth to auger refusal at the test hole locations ranged from 8.8 m to 10.2m

2.2 Groundwater Conditions

Four standpipe piezometers were installed at the locations of TH 11-08, 12, 21 and 26, to monitor the groundwater condition in the till. The groundwater levels are reported on the test hole logs. The groundwater levels range from elevation 235.27 m to 235.42 m at TH 11-12 and TH 11-08 respectively (measured Aug 10, 2011).

3. Foundation Alternatives

Driven Prestressed Precast Concrete (PPC) piles and cast in place friction piles are considered feasible alternatives to support the proposed buildings. Driven steel piles are considered not to be cost effective foundation alternative at this site. Shallow foundations are considered less suitable because of the depth to competent bearing stratum, long term settlement, associated excavation work, requirement for thermal insulation and potential impact on project schedule.

3.1 Driven Prestressed Precast Concrete (PPC)

The subsurface conditions at the site are suitable for driven PPC piles bearing into the dense glacial till. PPC piles can be designed on the basis of the conventional allowable capacities shown in Table 01 provided the piles are driven to the corresponding set criteria. The piles should be driven using a hammer with a rated energy of at least 40 kJ.

Table 01: Maximum Allowable Capacities for PPC Piles

PPC Pile Diameter (mm)	Maximum Allowable Capacity (kN)	Set Criteria (blows/25 mm)
300	450	5
350	625	8
400	800	12

Final set for driven PPC piles should be taken as three consecutive sets criteria as defined in the table above. PPC piles driven to the above criteria will develop the majority of their capacity from toe resistance, and therefore, no reduction in pile capacity is necessary for reasons related to group action. The design capacity of a pile group can be taken as the number of piles in the group multiplied by the allowable capacity per pile.

Further design and construction recommendations for PPC piles are summarized below:

- The weight of the embedded portion of the pile may be neglected in the design.
- The above allowable values pertain to soil resistance only. The pile cross sections must be designed to withstand the design loads and the driving forces during installation.
- Pile spacing should not be less than 2.5 pile diameters, measured center to center.
- Pre-boring not greater than 4 m may be use at all driven pile locations, to enhance pile plumbness and alignment, and to reduce the effects of pile heave during driving of adjacent piles. The diameter of the pre-bore hole should not exceed the nominal diameter of the pre-cast concrete pile. All piles should be driven continuously to the final set, once driving is initiated.
- All piles driven within 5 pile diameters should be monitored for heave and where heave is observed, the piles should be re-driven. Piles that are re-driven should be driven to the set criteria outlined above (i.e. re-drive piles for one full set).
- Any piles that are damaged, excessively out of plumb or refuse prematurely due to encountering boulders in the till may need to be replaced, pending a review of their load carrying capacity and expected settlement by a qualified geotechnical engineer.
- Where a steel follower is used to install the pre-cast concrete piles below ground surface, the set criteria may need to be adjusted to account for anticipated energy losses through the use of the follower. Adjustments to the set criteria should be determined by a qualified geotechnical engineer based on the site conditions, installation procedure and pile driving equipment.
- The driving of all piles should be documented by competent and knowledgeable geotechnical personnel.
- Sulphate resistant cement (Type HS) should be used for all concrete in contact with the soil.

- PDA testing is recommended to confirm efficiency of the pile driving system, assess driving stresses and evaluate pile capacity.

3.2 Cast-In-Place Friction Piles

Friction piles can be used to support lightly loaded structures. Frictional resistance from the top 3 m of the soil profile for exterior piles and the top 2 m of soil profile for the interior piles should not be counted towards the pile capacity due to potential volume change of soil and impact on soil/pile adhesion. The piles should not penetrate the till deposit to protect against groundwater infiltration, and the pile bore should be terminated at least 1.5 m above the clay/ till interface. Selection of the pile length should recognize the depth to till and the requirements to protect against upward seepage and hydraulic fracturing due to artesian water conditions in the till. Due to the location of the test holes in relation to the proposed building, the depth to till has not been determined at the final location of the proposed building. The shear strength tests were also performed on samples that are not in the immediate vicinity of the proposed building.

Table 02 provides values for the allowable unit skin friction resistance.

Table 02. Allowable Unit Skin Friction for Cast-In-Place Friction Piles

Zone (m below grade)	Allowable Skin Friction (kPa)
Exterior of Building	
0-3	0
3-7	12 kPa
Below 7 m	10 kPa
Interior of Building	
0-2	0
2-7	12 kPa
Below 7 m	10 kPa

Further design and construction recommendations for cast-in-place friction piles are summarized below:

- Minimum pile diameter of 600 mm is recommended.
- Pile spacing should not be less than 3 pile diameters, measured center to center.
- The embedded pile length should not be less than 6 m, however the pile length should be designed to provide adequate lateral and uplift resistance. Allowable uplift resistance equal 2/3 of the values shown in Table 02 can be used in the design. The pile design should include adequate steel reinforcement to withstand applicable loading conditions.
- Temporary sleeves may be required to protect against bore sloughing, and groundwater intrusion. The concrete should be placed immediately after completion of drilling.

- The pile bore should be pumped dry prior to concrete placement. If this cannot be achieved, the concrete should be placed using tremie methods.
- Sulphate resistant cement (Type HS) should be used for all concrete in contact with the soil.
- Pile installation should be documented by competent and knowledgeable geotechnical personnel.

4. Storm-water Retention Ponds

A cut slope of 6 Horizontal to 1 Vertical (6H:1V) is considered acceptable for the storm-water retention basins and is expected to perform satisfactorily. For stability reason, the crest of the cut slope (edges of the excavation) should be a minimum 8 m and 12 m away from the toe of the side and backstop berms respectively.

Base heave analysis considered the prevailing groundwater condition in the underlying till unit and the potential for hydraulic fracturing or heaving of the base of the excavation. The critical condition is during construction when there would be no water in the excavations. A factor of safety (FS) of 1.2 against base heave is considered acceptable for short term condition (during construction) and was used for the analysis. To maintain this design objective (FS = 1.2), the excavations for the storm-water retention ponds should not extend below elevation 233.2 m. The factor of safety against base heave will improve once the retention ponds are filled with water, therefore the ponds should be used as soon as practical. Every effort should be directed towards minimizing the duration of the excavation.

The excavation bottom will be below the measured groundwater levels in the till and the potential for upward seepage along existing natural fractures within the clay unit cannot be ruled out. Therefore requirements for construction dewatering should be allowed for in the construction budget and schedule.

Dewatering of the ponds after commissioning should be avoided due to concerns with cut slope stability and base heave. If complete dewatering of the ponds is required, the water level should be lowered at such a rate to protect against rapid drawdown effects. Rapid drawdown analysis has not been performed.

The potential for contamination of the aquifer by the retained water is beyond the scope of this report. An assessment by environmental and hydro-geological personnel is recommended.

5. Berms and Flood Protection Dikes

Three types of embankments are required at the site:

- 6.7 m high backstop berms, with a front face slope of 3H:2V
- 4.3 m high side berms, with a front face slope of 3H:2V
- Flood protection dikes, typically less than 1.5 m in height

The stability of the berm slopes was assessed using limit equilibrium slope stability analysis. A design objective factor of safety of 1.3 has been selected, taking into account the low consequence associated with slope instabilities if any. The parameters used in the analysis are summarized in

Table 03. The results of the stability assessment and the berm configurations are presented graphically in Appendix B and summarized in Table 04.

Table 03: Soil Parameters used in Stability Analysis

Material	Friction Angle (°)	Cohesion (kPa)	Unit Weight (kN/m³)
Native Clay	14	5	17
Compacted Clay Fill	20	5	19
Sand	32	0	19

Table 04: Results of Stability Analysis

Case	Calculated FS
Backstop Berm	
Interior Slope	1.33
Sand Facing ¹	±1.0
Exterior Slope	1.34
Exterior Slope 12 m pond set back - during construction	1.26
Exterior Slope 12 m pond setback - normal pond level	1.31
Side Berm	
Interior Slope	1.31
Exterior Slope	1.37
Exterior Slope 8 m pond set back - during construction	1.23
Exterior Slope 8 m pond setback - normal pond level	1.30

¹Stability of sand facing is near 1.0 because the required 3H:2V slope is near the angle of repose for loose sand.

Settlement of the berms is anticipated due to consolidation and elastic compression. The berm heights have been set so that the required minimum height should be maintained after the settlement has occurred.

The berms should be constructed of compacted clay. Organic soils should be removed beneath the footprint of the berms, and the surface of the sub grade should be scarified and compacted so that it is free of any soft areas. Sub grade improvement will be required under the steep slopes, a sub cut should be excavated to a depth of 0.6 m, and replaced with compacted clay material. The berm fill should be compacted to a minimum 95 percent of the Standard Procter maximum dry density (SPMDD).

If significant deformation (squeezing and bulking) of the subgrade occurs, compaction should be halted and an investigation undertaken to determine the cause of the deformation. If silt or silty material is encountered it should be overexcavated up to 0.75 m and bridged with geotextile and granular fill.

A 1 m thick facing of ballistic sand is required for the first 3 m above final grade, as a backstop behind the targets. This sand facing will be periodically removed and filtered to remove lead bullets. The 3H:2V slope of sand facing will be subject to surface ravelling, slumping, erosion and degradation due

to bullet impacts, precipitation, wind and other factors, and will require periodic maintenance. The 3H:2V facing of the backstop slope is a requirement of firing range design.

Drainage should be provided at the toe of the embankments and along the benches of the side and backstop berms to quickly remove surface water, and prevent any ponding of water on or against the berm.

The flood protection dikes should be constructed of compacted clay and have a minimum slope of 3H:1V and a minimum crest width of 1.5 m. Compaction of these dikes is necessary to provide effective flood protection. The subgrade should be prepared as described above.

6. Slabs-On-Grade

It is understood that a slab-on-grade floor system is preferred for economic and constructability reasons. While a structural floor is considered to provide better performance, a slab on grade floor system may be suitable for lightly loaded buildings where some movement of the floor is acceptable.

Floor slabs may be subjected to some vertical deformation due to swelling or shrinkage of the subgrade soil in response to changes in moisture content. Some settlement and differential settlement may also occur due to floor loading; uneven floor loading may lead to differential settlements. It is understood that the building will be heated during the winter months, and therefore, frost upheaval should not be a concern. The following are guidelines for design and construction of slab-on-grade:

1. The top 600 mm of the subgrade beneath the underside of the floor slab should be excavated and if found suitable can be used to backfill the subcut. The backfill should be placed in lift not to exceed 200 mm thick and compacted to a minimum 95 percent of SPMDD.
2. Precautions should be taken to prevent desiccation of clay subgrade during construction. If the soil does dry out, it should be dampened, scarified, and re-compacted to a minimum of 95 percent of Standard Proctor maximum dry density.
3. Any fill required to bring slab areas to design grade should consist of clean, inorganic material compacted to 95 percent of SPMDD.
4. A minimum of 150mm compacted thickness of clean free draining granular fill compacted to 98 percent of SPMDD should underlie the slab.
5. A vapour barrier below the slab is recommended, to minimize long term moisture change within the subgrade.
6. Competent subfloor drainage system should be provided for any portion of the slab which is constructed below the exterior grade.
7. The slab should be isolated from all fixed structural elements.
8. Light partitions bearing on the slab should be designed to permit vertical movement between the partition and the ceiling to minimize the possibility of damage if the slab heaves.

9. Control joints should be provided in the slab to reduce random cracking.
10. A minimum void space of 150 mm should be provided under grade beam system to minimize the effect of local soil movement.

7. Roadwork

The existing dirt road will be upgraded with a gravel surface and increased width to handle the anticipated vehicle types and volumes. The existing road embankment material is considered to be suitable sub-grade material for the upgraded roadway. The design of the pavement structure is being developed by others.

The slopes of the existing embankment should be benched prior to placing additional fill. Any topsoil encountered at the surface should be excavated and removed. The top 300 mm below the subgrade interface should be scarified and compacted to a minimum of 95 percent of SPMDD. If significant deformation (squeezing and bulking) of the subgrade occurs, compaction should be halted and an investigation undertaken to determine the cause of the deformation. If silt or silty material is encountered it should be over excavated up to 0.75 m and bridged with geotextile and granular fill. Side ditches should be provided on both sides to facilitate drainage and protect against saturation of the subgrade or pavement structure.

8. Parking Areas

Parking areas should be stripped of all organic material. The top 300 mm below the subgrade should be scarified and compacted to a minimum of 95 percent of SPMDD. If significant deformation (squeezing and bulking) of the subgrade occurs, compaction should be halted and an investigation undertaken to determine the cause of the deformation. A geotextile should be placed between the subgrade and subbase. The parking lot structure and on-site roadways should consist of 375 mm of granular sub base material, overlain by 150 mm of limestone base course. Parking lot grading should be designed so that surface water drains away from the parking lot, and does not drain or accumulate towards/under the pavement structure.

9. Closure

The findings and recommendations of this report were based on the results of the field and laboratory investigations. If conditions are encountered that appear to be different from those shown by the test holes drilled at this site and described in this report, or the assumptions stated herein are not in keeping with the design, this office should be notified in order that the recommendations can be reviewed and adjusted if necessary.

Soil conditions, by their nature, can be highly variable across a site. A contingency should be included in the construction budget to allow for the possibility of variation in soil conditions, which may result in modification of the design and construction procedures.

Sincerely,
AECOM Canada Ltd.

Submitted By:



Kendall Thiessen, P.Eng.
Geotechnical Engineer



Reviewed By:



Faris Khalil, P.Eng.
Manager, Geotechnical Engineering

Encl.

Statement of Qualifications and Limitations

The attached Report (the "Report") has been prepared by AECOM Canada Ltd. ("Consultant") for the benefit of the client ("Client") in accordance with the agreement between Consultant and Client, including the scope of work detailed therein (the "Agreement").

The information, data, recommendations and conclusions contained in the Report (collectively, the "Information"):

- is subject to the scope, schedule, and other constraints and limitations in the Agreement and the qualifications contained in the Report (the "Limitations")
- represents Consultant's professional judgement in light of the Limitations and industry standards for the preparation of similar reports
- may be based on information provided to Consultant which has not been independently verified
- has not been updated since the date of issuance of the Report and its accuracy is limited to the time period and circumstances in which it was collected, processed, made or issued
- must be read as a whole and sections thereof should not be read out of such context
- was prepared for the specific purposes described in the Report and the Agreement
- in the case of subsurface, environmental or geotechnical conditions, may be based on limited testing and on the assumption that such conditions are uniform and not variable either geographically or over time

Consultant shall be entitled to rely upon the accuracy and completeness of information that was provided to it and has no obligation to update such information. Consultant accepts no responsibility for any events or circumstances that may have occurred since the date on which the Report was prepared and, in the case of subsurface, environmental or geotechnical conditions, is not responsible for any variability in such conditions, geographically or over time.

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- as agreed in writing by Consultant and Client
- as required by law
- for use by governmental reviewing agencies

Statement of Qualifications and Limitations

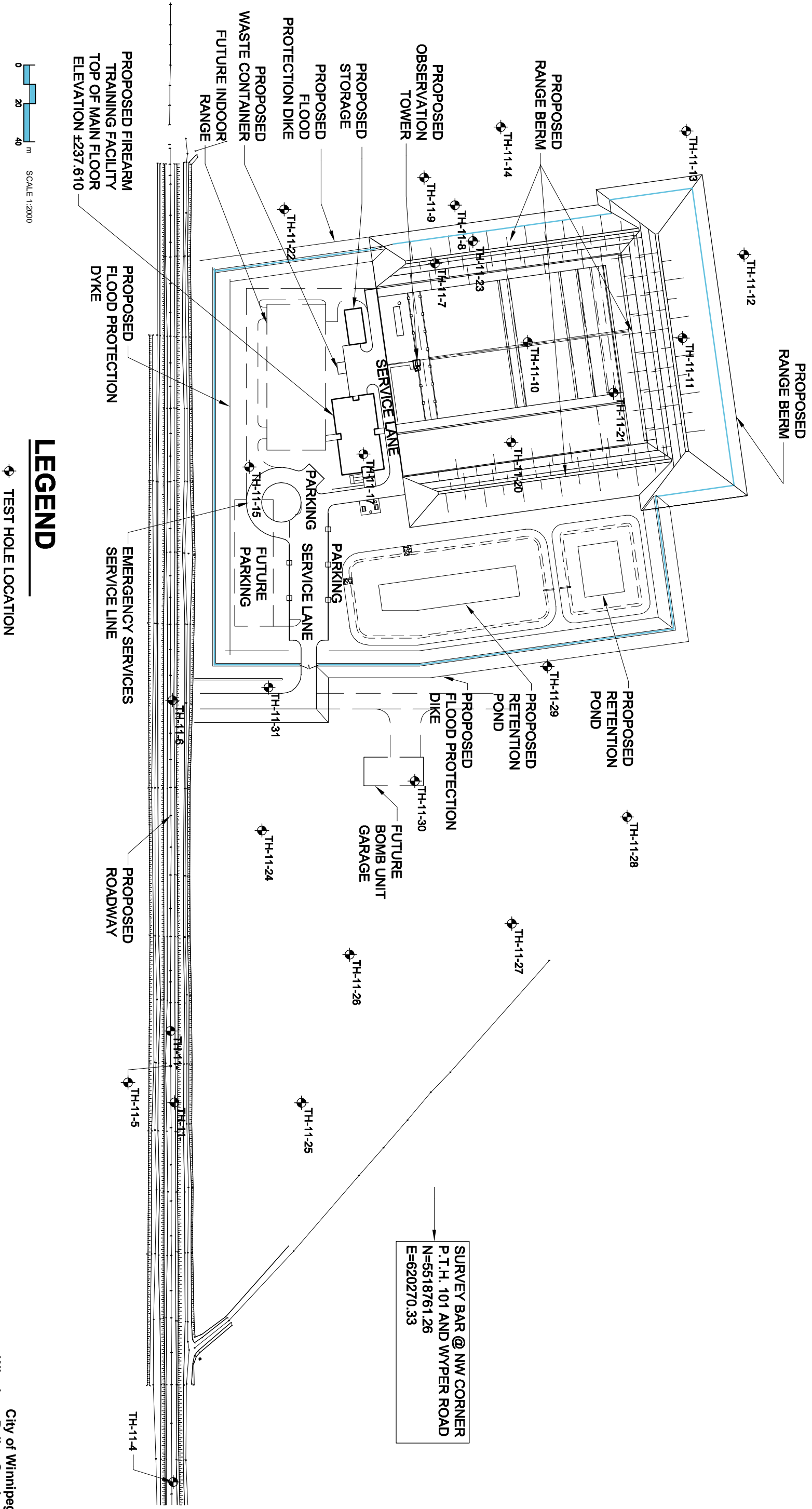
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Figures

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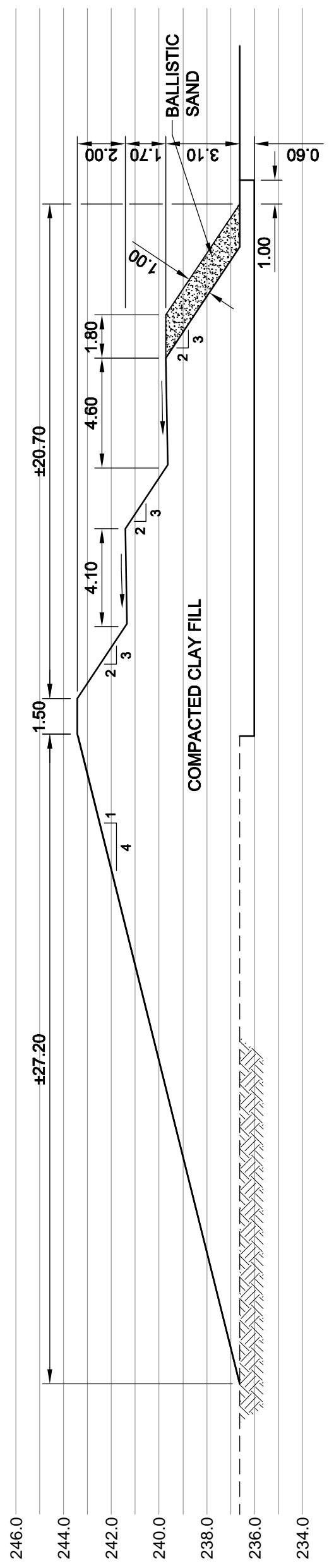


LEGEND

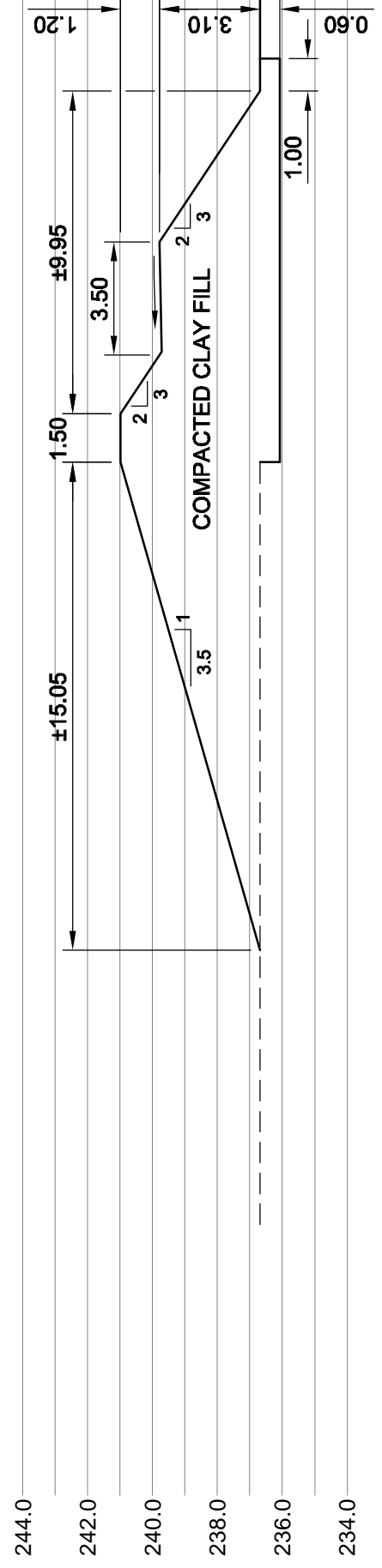
● TEST HOLE LOCATION



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BACKSTOP SECTION



SIDE BERM SECTION





Appendix A

AECOM Canada Ltd.

GENERAL STATEMENT

NORMAL VARIABILITY OF SUBSURFACE CONDITIONS

The scope of the investigation presented herein is limited to an investigation of the subsurface conditions as to suitability for the proposed project. This report has been prepared to aid in the evaluation of the site and to assist the engineer in the design of the facilities. Our description of the project represents our understanding of the significant aspects of the project relevant to the design and construction of earth work, foundations and similar. In the event of any changes in the basic design or location of the structures as outlined in this report or plan, we should be given the opportunity to review the changes and to modify or reaffirm in writing the conclusions and recommendations of this report.

The analysis and recommendations presented in this report are based on the data obtained from the borings and test pit excavations made at the locations indicated on the site plans and from other information discussed herein. This report is based on the assumption that the subsurface conditions everywhere are not significantly different from those disclosed by the borings and excavations. However, variations in soil conditions may exist between the excavations and, also, general groundwater levels and conditions may fluctuate from time to time. The nature and extent of the variations may not become evident until construction. If subsurface conditions differ from those encountered in the exploratory borings and excavations, are observed or encountered during construction, or appear to be present beneath or beyond excavations, we should be advised at once so that we can observe and review these conditions and reconsider our recommendations where necessary.

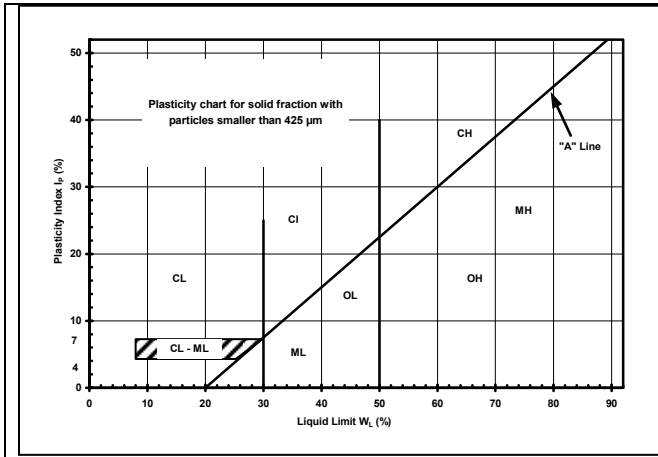
Since it is possible for conditions to vary from those assumed in the analysis and upon which our conclusions and recommendations are based, a contingency fund should be included in the construction budget to allow for the possibility of variations which may result in modification of the design and construction procedures.

In order to observe compliance with the design concepts, specifications or recommendations and to allow design changes in the event that subsurface conditions differ from those anticipated, we recommend that all construction operations dealing with earth work and the foundations be observed by an experienced soils engineer. We can be retained to provide these services for you during construction. In addition, we can be retained to review the plans and specifications that have been prepared to check for substantial conformance with the conclusions and recommendations contained in our report.

EXPLANATION OF FIELD & LABORATORY TEST DATA

Description			UMA Log Symbols	USCS Classification	Laboratory Classification Criteria				
					Fines (%)	Grading	Plasticity	Notes	
COARSE GRAINED SOILS	GRAVELS (More than 50% of coarse fraction of gravel size)	CLEAN GRAVELS (Little or no fines)	Well graded gravels, sandy gravels, with little or no fines		GW	0-5	$C_u > 4$ $1 < C_c < 3$	Dual symbols if 5-12% fines. Dual symbols if above "A" line and $4 < W_p < 7$ $C_u = \frac{D_{60}}{D_{10}}$ $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$	
			Poorly graded gravels, sandy gravels, with little or no fines		GP	0-5	Not satisfying GW requirements		
		DIRTY GRAVELS (With some fines)	Silty gravels, silty sandy gravels		GM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey gravels, clayey sandy gravels		GC	> 12			Atterberg limits above "A" line or $W_p < 7$
	SANDS (More than 50% of coarse fraction of sand size)	CLEAN SANDS (Little or no fines)	Well graded sands, gravelly sands, with little or no fines		SW	0-5	$C_u > 6$ $1 < C_c < 3$		
			Poorly graded sands, gravelly sands, with little or no fines		SP	0-5	Not satisfying SW requirements		
		DIRTY SANDS (With some fines)	Silty sands, sand-silt mixtures		SM	> 12			Atterberg limits below "A" line or $W_p < 4$
			Clayey sands, sand-clay mixtures		SC	> 12			Atterberg limits above "A" line or $W_p < 7$
FINE GRAINED SOILS	SILTS (Below 'A' line negligible organic content)	$W_L < 50$	Inorganic silts, silty or clayey fine sands, with slight plasticity		ML		Classification is Based upon Plasticity Chart		
		$W_L > 50$	Inorganic silts of high plasticity		MH				
	CLAYS (Above 'A' line negligible organic content)	$W_L < 30$	Inorganic clays, silty clays, sandy clays of low plasticity, lean clays		CL				
		$30 < W_L < 50$	Inorganic clays and silty clays of medium plasticity		CI				
		$W_L > 50$	Inorganic clays of high plasticity, fat clays		CH				
	ORGANIC SILTS & CLAYS (Below 'A' line)	$W_L < 50$	Organic silts and organic silty clays of low plasticity		OL				
		$W_L > 50$	Organic clays of high plasticity		OH				
	HIGHLY ORGANIC SOILS		Peat and other highly organic soils		Pt	Von Post Classification Limit		Strong colour or odour, and often fibrous texture	
	Asphalt		Till			AECOM			
	Concrete		Bedrock (Undifferentiated)						
	Fill		Bedrock (Limestone)						

When the above classification terms are used in this report or test hole logs, the designated fractions may be visually estimated and not measured.



FRACTION	SEIVE SIZE (mm)		DEFINING RANGES OF PERCENTAGE BY WEIGHT OF MINOR COMPONENTS		
	Passing	Retained	Percent	Identifier	
Gravel	Coarse	76	19	35-50	and
	Fine	19	4.75		
Sand	Coarse	4.75	2.00	20-35	"y" or "ey" *
	Medium	2.00	0.425		
	Fine	0.425	0.075		
Silt (non-plastic) or Clay (plastic)	< 0.075 mm		10-20	1-10	some
			1-10		
* for example: gravelly, sandy clayey, silty					
Definition of Oversize Material					
COBBLES: 76mm to 300mm diameter					
BOULDERS: >300mm diameter					

LEGEND OF SYMBOLS

Laboratory and field tests are identified as follows:

- qu - undrained shear strength (kPa) derived from unconfined compression testing.
- Tv - undrained shear strength (kPa) measured using a torvane
- pp - undrained shear strength (kPa) measured using a pocket penetrometer.
- Lv - undrained shear strength (kPa) measured using a lab vane.
- Fv - undrained shear strength (kPa) measured using a field vane.
- γ - bulk unit weight (kN/m³).
- SPT - Standard Penetration Test. Recorded as number of blows (N) from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 51 mm O.D. Raymond type sampler 0.30 m into the soil.
- DPPT - Drive Point Pentrometer Test. Recorded as number of blows from a 63.5 kg hammer dropped 0.76 m (free fall) which is required to drive a 50 mm drive point 0.30 m into the soil.
- w - moisture content (WL, Wp)

The undrained shear strength (Su) of a cohesive soil can be related to its consistency as follows:

Su (kPa)	CONSISTENCY
<12	very soft
12 – 25	soft
25 – 50	medium or firm
50 – 100	stiff
100 – 200	very stiff
200	hard

The resistance (N) of a non-cohesive soil can be related to compactness condition as follows

N – BLOWS/0.30 m	COMPACTNESS
0 - 4	very loose
4 - 10	loose
10 - 30	compact
30 - 50	dense
50	very dense

PROJECT: Wyper Road Firearms Training Facility	CLIENT: Winnipeg Police Services	TESTHOLE NO: TH11-04
LOCATION: On Wyper Road - N 5518744.62 / E 620169.31		PROJECT NO.: 60162215
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Acker MP-5 125 mm SSA	ELEVATION (m): 237.39
SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB <input type="checkbox"/> SHELBY TUBE <input checked="" type="checkbox"/> SPLIT SPOON <input type="checkbox"/> BULK <input checked="" type="checkbox"/> NO RECOVERY <input type="checkbox"/> CORE	

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ●	(kPa)			
0		TOPSOIL- organic, black, dry									237
0		CLAY (Fill) - silty, trace sand, trace gravel, grey, dry									
0.5		CLAY - silty - brown, moist, stiff - high plasticity		G1	~55						
1.5				G2	~55						
2.5		- firm below 2.4 m									235
3.5		- dark brown below 3.1 m		G3	~55						
4.5		- soft below 4.3 m		G4	~55						
5.5		- brown to grey below 4.6 m									232
6.0				G5	~55						
6.1		END OF TEST HOLE AT 6.1 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									231
7.0											230
8.0											229
9.0											228
10.0											227
11.0											226
12.0											225
12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar	COMPLETION DEPTH: 6.10 m
REVIEWED BY: Kendall Thiessen	COMPLETION DATE: 8/3/11
PROJECT ENGINEER: Kendall Thiessen	Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility	CLIENT: Winnipeg Police Services	TESTHOLE NO: TH11-05
LOCATION: On Wyper Road - N 5518741.28 / E 619969.03		PROJECT NO.: 60162215
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Acker MP-5 125 mm SSA	ELEVATION (m): 237.55
SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB <input type="checkbox"/> SHELBY TUBE <input checked="" type="checkbox"/> SPLIT SPOON <input type="checkbox"/> BULK <input checked="" type="checkbox"/> NO RECOVERY <input type="checkbox"/> CORE	

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ●				
0		TOPSOIL - organics, black, dry									237
0		CLAY (Fill) - silty, trace sand, trace gravel, trace rootlets, grey, dry									
0.5		CLAY - silty - grey, moist, stiff - high plasticity - trace rootlets - soft below 1.2 m		G6	~55						
1.5				G7	~45						236
3.1		- dark brown below 3.1 m		G8	~55						235
4.9		- soft below 4.9 m		G9	~55						233
5.6		- brown to grey below 5.6 m		G10	~55						232
6.1		END OF TEST HOLE AT 6.1 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									231
7											230
8											229
9											228
10											227
11											226

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar	COMPLETION DEPTH: 6.10 m
REVIEWED BY: Kendall Thiessen	COMPLETION DATE: 8/3/11
PROJECT ENGINEER: Kendall Thiessen	Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility	CLIENT: Winnipeg Police Services	TESTHOLE NO: TH11-06
LOCATION: On Wyper Road - N 5518738.02 / E 619762.84		PROJECT NO.: 60162215
CONTRACTOR: Maple Leaf Drilling Ltd.	METHOD: Acker MP-5 125 mm SSA	ELEVATION (m): 237.82
SAMPLE TYPE	<input checked="" type="checkbox"/> GRAB <input type="checkbox"/> SHELBY TUBE <input checked="" type="checkbox"/> SPLIT SPOON <input type="checkbox"/> BULK <input checked="" type="checkbox"/> NO RECOVERY <input type="checkbox"/> CORE	

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ● (kPa)			
0		TOPSOIL - organics, black, dry								
0		CLAY (Fill) - silty, trace sand, trace gravel, trace rootlets, black, dry								
0.5		CLAY - silty - black, dry, very stiff to soft - high plasticity - trace rootlets - trace rootlets		G11	~55					237
1.5		- brown, firm below 1.8 m		G12	~55					236
3.0				G13	~55					235
4.0		- brown to light grey below 3.7 m		G14	~55					234
5.5		- dark brown, soft below 5.5 m		G15	~55					233
6.1		END OF TEST HOLE AT 6.1 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.								232
7.0										231
8.0										230
9.0										229
10.0										228
11.0										227
12.0										226

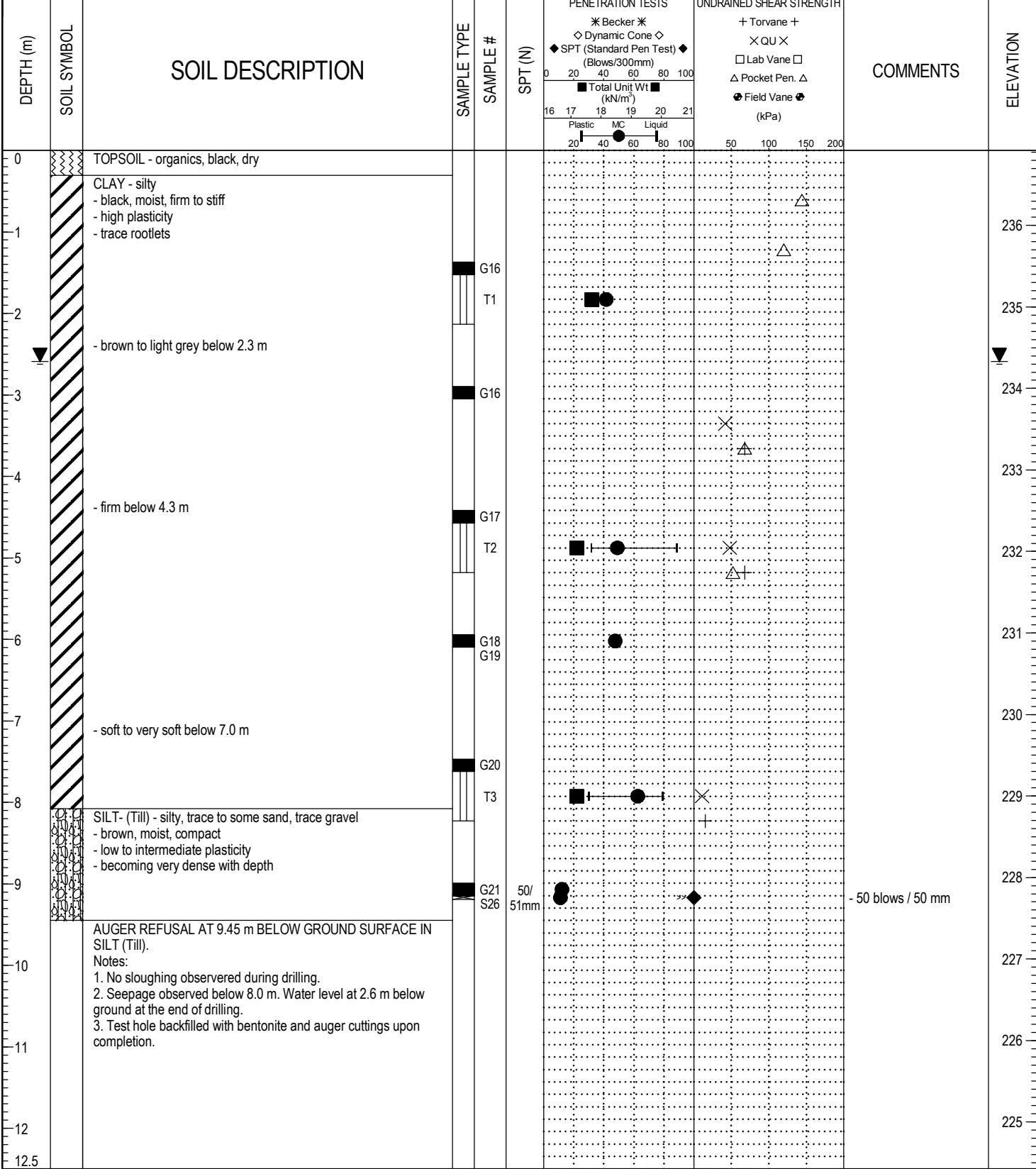
LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar	COMPLETION DEPTH: 6.10 m
REVIEWED BY: Kendall Thiessen	COMPLETION DATE: 8/3/11
PROJECT ENGINEER: Kendall Thiessen	Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-07
 LOCATION: N 5518864.77 / E 619538.64 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.92

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

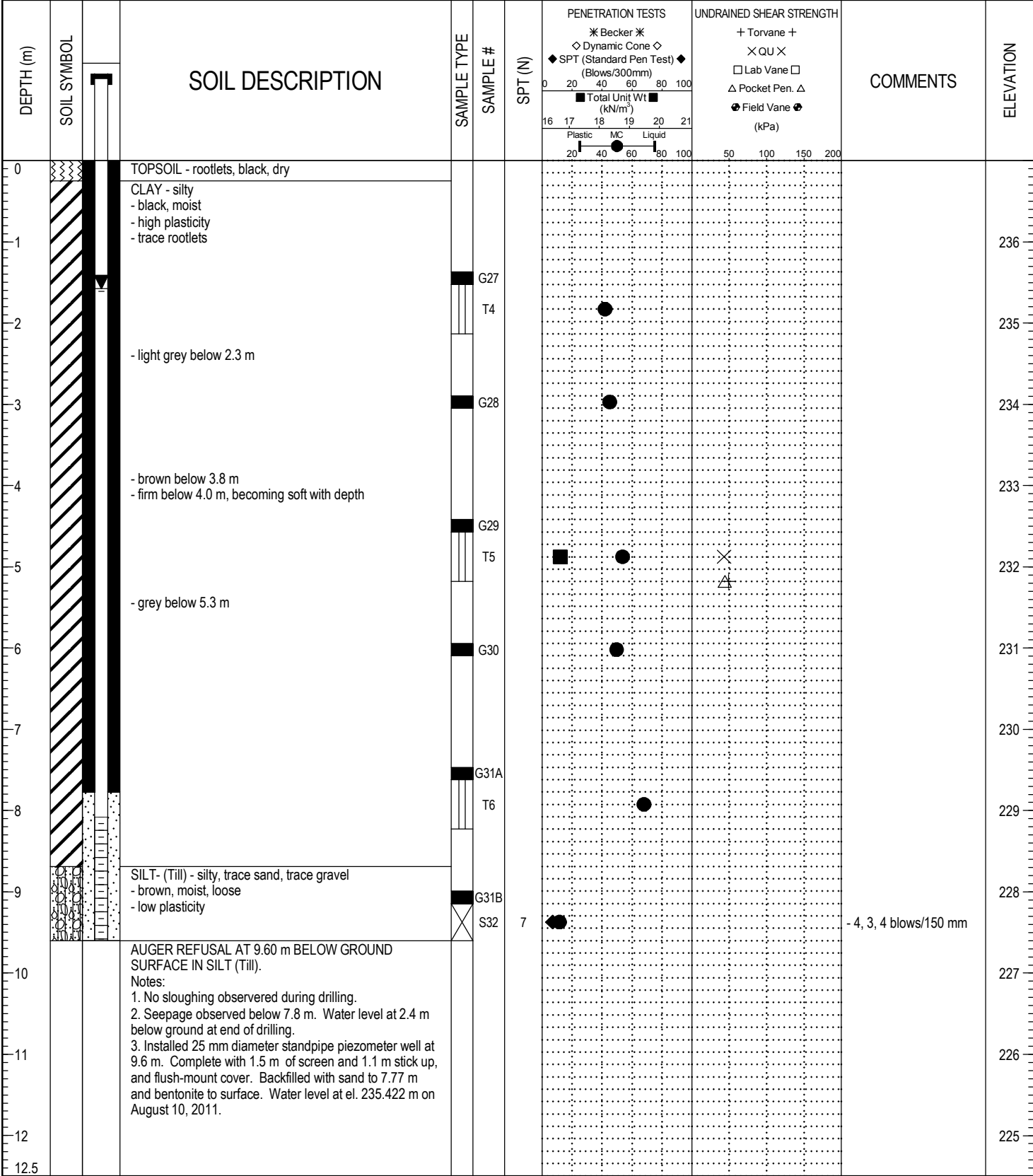


LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 9.45 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/3/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility		CLIENT: Winnipeg Police Services		TESTHOLE NO: TH11-08		
LOCATION: N 5518881.09 / E 619514.45		METHOD: Acker MP-5 125 mm SSA		PROJECT NO.: 60162215		
CONTRACTOR: Maple Leaf Drilling Ltd.		ELEVATION (m): 237.00				
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND



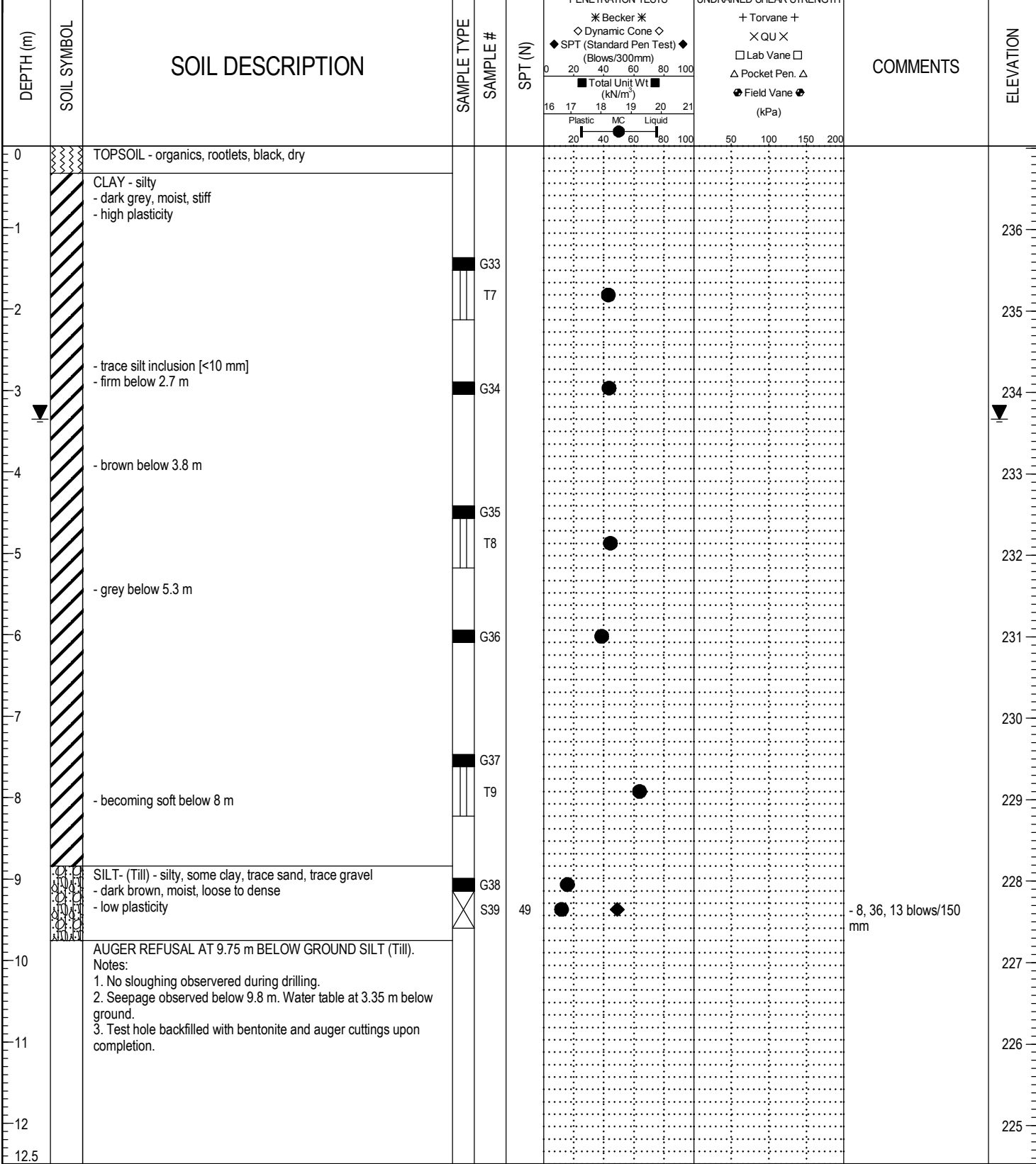
LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar	COMPLETION DEPTH: 9.60 m
REVIEWED BY: Kendall Thiessen	COMPLETION DATE: 8/3/11
PROJECT ENGINEER: Kendall Thiessen	Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-09
 LOCATION: N 5518863.36 / E 619505.73 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 237.03

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE



LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT- 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 9.75 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/3/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: **TH11-10**
 LOCATION: N 5518912.87 / E 619588.43 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.93

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Blows/300mm	Total Unit Wt (kN/m ³)	(kPa)	(kPa)		
0		TOPSOIL - organics, rootlets - black, dry									236
0		CLAY - silty - greyish brown, dry, stiff - high plasticity									
2.3		- light grey to grey brown below 2.3 m		G40	~55						235
2.7		- firm to soft below 2.7 m		G41A	~65						234
4.8				G41B G42	~75						232
5.5		- grey below 5.5 m		G43	~70						231
7.5				G44	~50						229
9.14		SILT- (Till) - silty, trace to some sand, trace to some gravel - brown to light grey, moist, loose to compact - low plasticity		G45	~45						228

END OF TEST HOLE AT 9.14 m BELOW GROUND SURFACE IN SILT (Till).
 Notes:
 1. No sloughing observed during drilling.
 2. Seepage observed in till. Water level at 2.4 m below ground at end of drilling.
 3. Test hole backfilled with bentonite and auger cuttings upon completion.

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 9.14 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-11
 LOCATION: N 5519002.05 / E 619581.4 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.84

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

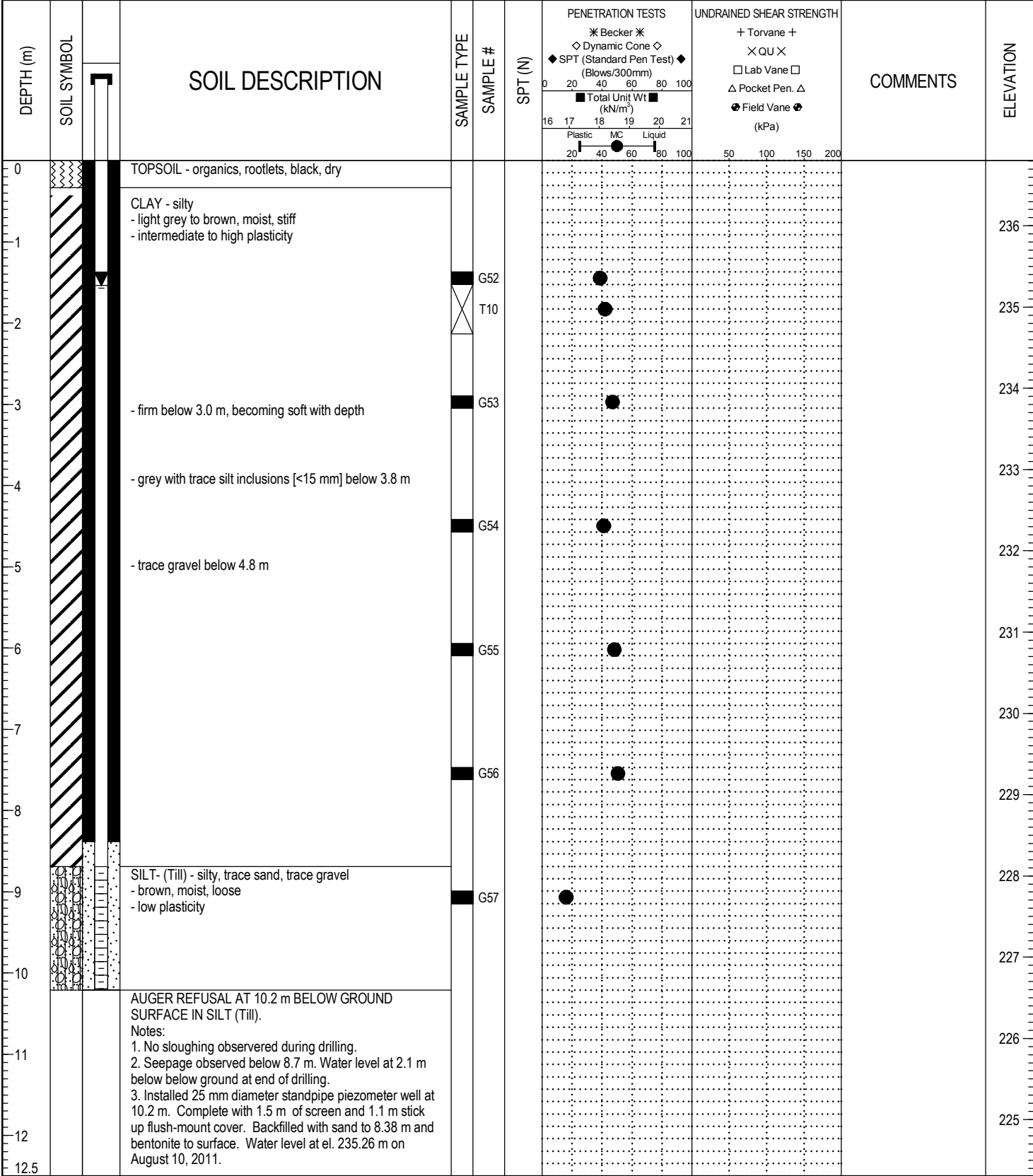
DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS	UNDRAINED SHEAR STRENGTH	COMMENTS	ELEVATION
0		TOPSOIL - organics, rootlets - black, dry							236
0-1		CLAY - silty - light grey, dry, stiff to soft - high plasticity - trace rootlets							
2.1		- becoming firm to soft below 2.1 m							
2.1-3.0				G46	~55				235
3.0-4.5				G47	~65				234
4.5-5.3				G48	~75				233
5.3-6.0				G49	~85				232
6.0-8.84		- grey below 5.3 m		G50	~95				231
8.84-9.0				G51	~105				230
9.0-9.1		SILT- (Till) - silty, trace to some sand, trace to some gravel - brown, moist, very soft - low plasticity							229
9.1-9.2		AUGER REFUSAL AT 8.84 m BELOW GROUND SURFACE IN SILT (Till).							228
9.2-12.5		Notes: 1. No sloughing observed during drilling. 2. Seepage observed below 8.5 m. Water level at 2.4 m below ground at end of drilling. 3. Test hole backfilled with bentonite and auger cuttings upon completion.							227

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT - 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 8.84 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility		CLIENT: Winnipeg Police Services		TESTHOLE NO: TH11-12		
LOCATION: N 5519032.99 / E 619527.39				PROJECT NO.: 60162215		
CONTRACTOR: Maple Leaf Drilling Ltd.			METHOD: Acker MP-5 125 mm SSA		ELEVATION (m): 236.80	
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND



LOGGED BY: M. Akhtar	COMPLETION DEPTH: 10.21 m
REVIEWED BY: Kendall Thiessen	COMPLETION DATE: 8/4/11
PROJECT ENGINEER: Kendall Thiessen	Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-13
 LOCATION: N 5519002.89 / E 619467.19 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.92

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU X Lab Vane □ Pocket Pen. Δ	Field Vane ●		
0		TOPSOIL - rootlets - grey to black, dry									
0-1		CLAY - silty - light grey to grey, dry, stiff - intermediate plasticity - brown below 1.1 m									236
1-2				G58	~55						235
2-3				G59	~55						234
3-4				G60	~55						233
4-5				G61	~55						232
5-6		- dark grey to grey, firm below 5.33 m		G62	~55						231
6-7				G63	~55						230
7-8		- soft below 6.8 m									229
8-9											228
9		SILT- (Till) - silty, trace sand, trace gravel - light grey to grey, moist, loose - low plasticity									227
9.14		AUGER REFUSAL AT 9.14 m BELOW GROUND SURFACE IN SILT (Till). Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									226
10											225
11											224
12											223
12.5											222

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 9.14 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-14
 LOCATION: N 5518907.81 / E 619467.19 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 237.08

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU × Lab Vane □ Pocket Pen. △ Field Vane ⊕	(kPa)		
0	TOPSOIL - rootlets, black to grey, dry										237
0-1	CLAY - silty - black, moist, stiff - high plasticity - trace organics - trace silt inclusions			G64	~55						236
1-2	- brown, firm to soft below 1.8 m			G65	~65						235
2-3				G66	~75						234
3-4				G67	~85						233
4-5				G68	~95						232
5-6				G69	~105						231
6-7	- dark grey below 6.8 m										230
7-8											229
8-9	SILT- (Till) - clayey, trace sand, trace gravel - brown to light grey, moist, soft - low to intermediate plasticity										228
9-10	END OF TEST HOLE AT 9.1 m BELOW GROUND SURFACE IN SILT (Till). Notes: 1. No sloughing observed during drilling. 2. Seepage observed below 8.5 m. Water level at 2.7 m below ground surface at end of drilling 3. Test hole backfilled with bentonite and auger cuttings upon completion.										227
10-11											226
11-12											225
12-12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 9.14 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-15
 LOCATION: N 5518777.37 / E 619656.19 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 237.04

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ●	(kPa)			
0		TOPSOIL - black to grey, dry									
0		CLAY - silty - grey, moist, very stiff - intermediate to high plasticity		G112	●						236
1				G113	●						235
2		END OF TEST HOLE AT 1.52 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									234
3											233
4											232
5											231
6											230
7											229
8											228
9											227
10											226
11											225
12											225
12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 1.52 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-17
 LOCATION: N 5518849.3 / E 619634.84 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.92

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU X Lab Vane □ Pocket Pen. Δ	Field Vane ⊗		
0		TOPSOIL - black, dry									
0		CLAY - silty - dark grey, moist, very stiff - becoming firm with depth - intermediate to high plasticity - trace rootlets		G114	~55						236
1		- grey to brown below 1.5 m - soft below 2.4 m		G115	~65						235
3				G116	~85						234
3.04		END OF TEST HOLE AT 3.04 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									233
4											232
5											231
6											230
7											229
8											228
9											227
10											226
11											225
12											225
12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-20
 LOCATION: N 5518907.53 / E 619643.85 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.93

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU X Lab Vane □ Pocket Pen. Δ	Field Vane ⊗		
0		TOPSOIL - black, dry									236
0-1		CLAY - silty - grey to black, moist, stiff, becoming firm with depth - intermediate to high plasticity - trace silt inclusions									
1-2.2		- brown below 2.2 m									
2.2-5.3		- brown to grey below 5.3 m									
5.3-6.1		END OF TEST HOLE AT 6.1 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									
6.1				G77	~55						235
				G78	~55						234
				G79	~55						232
				G80	~55						231

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 6.10 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility		CLIENT: Winnipeg Police Services		TESTHOLE NO: TH11-21		
LOCATION: N 5518966.88 / E 619614.31				PROJECT NO.: 60162215		
CONTRACTOR: Maple Leaf Drilling Ltd.			METHOD: Acker MP-5 125 mm SSA		ELEVATION (m): 236.94	
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker	Dynamic Cone	Torvane	QU		
0		TOPSOIL - rootlets - black, dry									236
0.5		CLAY - silty - grey to black, moist, stiff to soft - intermediate to high plasticity		G81							235
2.5				G82							234
3.8		- mottled brown and light grey below 3.8 m		G83							233
5.2		- grey below 5.2 m		G84							232
5.5		- soft below 5.5 m									231
7.0											230
8.8		SILT (Till) - some clay, some sand, trace gravel - light grey, compact, low plasticity									229
8.8		AUGER REFUSAL AT 8.8 m BELOW GROUND SURFACE IN SILT (Till). Notes: 1. No sloughing observed during drilling. 3. Seepage observed from till. Water level at 2.1 m below ground surface at end of drilling. 4. Installed 25 mm diameter standpipe piezometer well at 8.8 m. Complete with 1.5 m of screen and 1.0 m stick up flush-mount cover. Backfilled with sand to 7.01 m and bentonite to surface. Water level at el. 235.30 on August 10, 2011.									228
10.0											227
11.0											226
12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT - 9/16/11



LOGGED BY: M. Akhtar	COMPLETION DEPTH: 8.84 m
REVIEWED BY: Kendall Thiessen	COMPLETION DATE: 8/4/11
PROJECT ENGINEER: Kendall Thiessen	Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-22
 LOCATION: N 5518792.47 / E 619512.2 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.79

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ● (kPa)				
0		TOPSOIL - organics, black, dry									
0		CLAY - silty - grey to black, moist, stiff - intermediate to high plasticity - trace silt inclusions (<10 mm), trace rootlets - becoming firm with depth below 1.5 m		G85							236
1				G86							235
2											234
3		- dark brown to grey below 2.2 m		G87							233
3		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									232
4											231
5											230
6											229
7											228
8											227
9											226
10											225
11											225
12											225
12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-23
 LOCATION: N 5518895.43 / E 619532.73 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.92

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU X Lab Vane □ Pocket Pen. Δ	Field Vane ⊗		
0		TOPSOIL - organics, black, dry									
0		CLAY - silty - brown, moist, stiff - high plasticity - becoming firm below 2 m - trace silt inclusions									236
1				G70							235
2				G71							234
3				G72							233
4				G73							232
5		- grey below 5.3 m		G74							231
6				G75							230
7		- soft below 7 m		G76							229
8				G77							228
9		SILT- (Till) - silty, trace sand, trace gravel - light grey to grey, moist, very dense - low plasticity		G78							227
9.53		AUGER REFUSAL AT 9.52 m BELOW GROUND SURFACE IN SILT (Till). Notes: 1. No sloughing observed during drilling. 2. Seepage observed below 8.7 m. Water Level at 2.4 m below ground at end of drilling. 3. Test hole backfilled with bentonite and auger cuttings upon completion.		S76	55						226
10											225
11											224
12											223
12.5											222

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT - 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 9.53 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-24
 LOCATION: N 5518779.82 / E 619850.32 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.75

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ●	(kPa)			
0		TOPSOIL - organics, rootlets, black, dry									
0		CLAY - silty - dark grey to brown, moist, stiff - high plasticity		G88	~55						236
1				G89	~65						235
2											
3		- firm below 2.4 m		G90	~75						234
3		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									233
4											232
5											231
6											230
7											229
8											228
9											227
10											226
11											225
12											
12.5											

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-25
 LOCATION: N 5518809.35 / E 619983.94 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.68

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Blows/300mm	Total Unit Wt (kN/m ³)	Lab Vane	Field Vane		
0		TOPSOIL - rootlets, black, dry									236
0-1		CLAY - silty - grey, moist, stiff - high plasticity	<input checked="" type="checkbox"/>	G91	~50						236
1-2			<input checked="" type="checkbox"/>	G92	~55						235
2-3		- firm below 2.4 m									234
3		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.	<input checked="" type="checkbox"/>	G93	~60						233
3-4											232
4-5											231
5-6											230
6-7											229
7-8											228
8-9											227
9-10											226
10-11											225
11-12											224
12-12.5											223

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility		CLIENT: Winnipeg Police Services		TESTHOLE NO: TH11-26		
LOCATION: N 5518838.05 / E 619889.14				PROJECT NO.: 60162215		
CONTRACTOR: Maple Leaf Drilling Ltd.			METHOD: Acker MP-5 125 mm SSA		ELEVATION (m): 236.69	
SAMPLE TYPE	GRAB	SHELBY TUBE	SPLIT SPOON	BULK	NO RECOVERY	CORE
BACKFILL TYPE	BENTONITE	GRAVEL	SLOUGH	GROUT	CUTTINGS	SAND

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Blows/300mm	Total Unit Wt (kN/m ³)	+	+		
0		TOPSOIL - rootlets, black, dry									
0.5		CLAY - silty - grey, moist, stiff to soft - high plasticity - trace silt inclusions (<15 mm)		G94							236
1.5				G95							235
2.0		- mottled grey and brown, soft below 1.8 m									234
3.0				G96							233
4.0											232
5.0											231
6.0											230
7.0											229
8.0											228
8.8		SILT (Till) - some sand, trace gravel - compact, low plasticity									227
9.0		AUGER REFUSAL AT 8.8 m BELOW GROUND SURFACE IN CLAY.									226
10.0		Notes: 1. No sloughing observed during drilling. 2. No seepage observed during drilling. 3. Installed 25 mm diameter standpipe piezometer well at 8.8 m. Complete with 1.5 m of screen and 1.0 m stick up flush-mount cover. Backfilled with sand to 7.01 m and bentonite to surface. Water level at el. 235.30 on August 10, 2011.									225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT - 9/16/11



LOGGED BY: M. Akhtar	COMPLETION DEPTH: 3.05 m
REVIEWED BY: Kendall Thiessen	COMPLETION DATE: 8/4/11
PROJECT ENGINEER: Kendall Thiessen	Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-27
 LOCATION: N 5518912.59 / E 619887.46 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.74

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ● (kPa)				
0		TOPSOIL - organics, rootlets, black, dry									
0		CLAY - silty - dark grey, moist, stiff to soft - high plasticity - trace silt inclusions [<10 mm] - light grey - grey to light grey below 1.5 m		G97	55						236
1				G98	55						235
3					G99	55					
3		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No Sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									233
4											232
5											231
6											230
7											229
8											228
9											227
10											226
11											225
12											225
12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-28
 LOCATION: N 5518973.07 / E 619832.32 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.82

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU × Lab Vane □ Pocket Pen. △ Field Vane ⊗	(kPa)		
0		TOPSOIL - organics, black, dry									
0.5		CLAY - silty - mottled black and grey, moist, stiff becoming firm with depth - intermediate to high plasticity - trace silt inclusions [<10 mm]		G100	~55						236
1.0				G101	~65						235
2.0		- brown below 2 m									234
2.3		- soft below 2.3 m									233
3.0		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No Sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.		G102	~75						232
4.0											231
5.0											230
6.0											229
7.0											228
8.0											227
9.0											226
10.0											225
11.0											225
12.0											225
12.5											225

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-29
 LOCATION: N 5518938.75 / E 619757.49 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.64

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m ³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ●	(kPa)			
0	TOPSOIL - black, dry										
0	CLAY - silty - grey to dark grey, moist, stiff to soft - intermediate plasticity - trace silt inclusions [< 8 mm], trace rootlets			G103	~55						236
1			G104	~55							235
3			G105	~55							234
3		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									233
4											232
5											231
6											230
7											229
8											228
9											227
10											226
11											225
12											
12.5											

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-30
 LOCATION: N 5518861.39 / E 619810.94 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.70

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						Becker * Dynamic Cone ◊ SPT (Standard Pen Test) ◆ (Blows/300mm)	Total Unit Wt (kN/m ³)	Torvane + QU X Lab Vane □ Pocket Pen. Δ	Field Vane ⊕		
0		TOPSOIL- black, dry									
0-1		CLAY - silty - brown to black, dry, stiff to soft - high plasticity - trace silt inclusions [< 20 mm]	<input checked="" type="checkbox"/>	G106	~55						236
1-2			<input checked="" type="checkbox"/>	G107	~65						235
2-3		- grey below 2.2 m									234
3		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.	<input checked="" type="checkbox"/>	G108	~75						233
3-4											232
4-5											231
5-6											230
6-7											229
7-8											228
8-9											227
9-10											226
10-11											225
11-12											224
12-12.5											223

LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1

PROJECT: Wyper Road Firearms Training Facility CLIENT: Winnipeg Police Services TESTHOLE NO: TH11-31
 LOCATION: N 5518795.85 / E 619772.68 PROJECT NO.: 60162215
 CONTRACTOR: Maple Leaf Drilling Ltd. METHOD: Acker MP-5 125 mm SSA ELEVATION (m): 236.87

SAMPLE TYPE GRAB SHELBY TUBE SPLIT SPOON BULK NO RECOVERY CORE

DEPTH (m)	SOIL SYMBOL	SOIL DESCRIPTION	SAMPLE TYPE	SAMPLE #	SPT (N)	PENETRATION TESTS		UNDRAINED SHEAR STRENGTH		COMMENTS	ELEVATION
						* Becker * ◇ Dynamic Cone ◇ ◆ SPT (Standard Pen Test) ◆ (Blows/300mm) ■ Total Unit Wt (kN/m³)	+ Torvane + × QU × □ Lab Vane □ △ Pocket Pen. △ ● Field Vane ●	(kPa)			
0		TOPSOIL - black, dry									
0		CLAY - silty - mottled dark grey to black, dry, very stiff to soft - intermediate plasticity		G109							236
1				G110							235
2											234
3		- brown below 2.3 m		G111							233
3		END OF TEST HOLE AT 3 m BELOW GROUND SURFACE IN CLAY. Notes: 1. No sloughing observed during drilling. 2. No seepage observed. 3. Test hole backfilled with bentonite and auger cuttings upon completion.									232
4											231
5											230
6											229
7											228
8											227
9											226
10											225
11											225
12											225
12.5											225

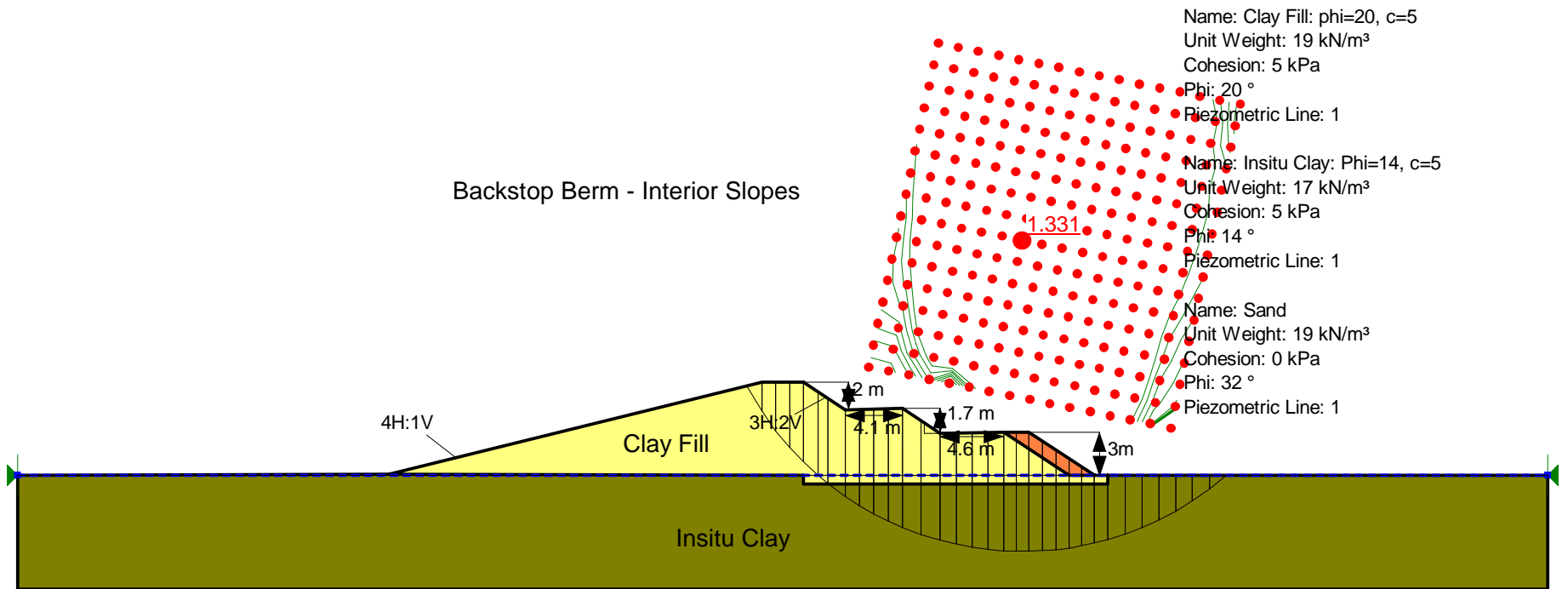
LOG OF TEST HOLE 60162215 BOREHOLE LOGS - WYPER RD.GPJ UMA WINN.GDT 9/16/11



LOGGED BY: M. Akhtar COMPLETION DEPTH: 3.05 m
 REVIEWED BY: Kendall Thiessen COMPLETION DATE: 8/4/11
 PROJECT ENGINEER: Kendall Thiessen Page 1 of 1



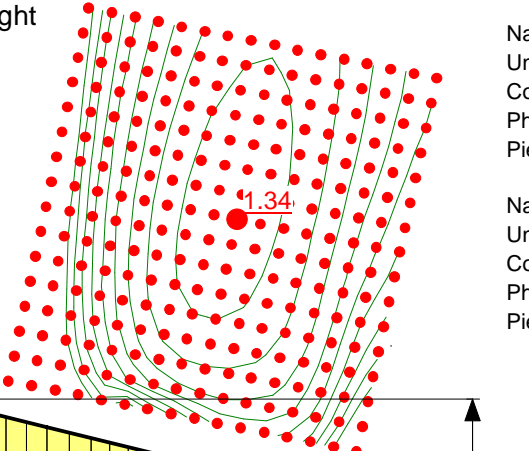
Appendix B



Backstop Berm - 6.7m height
Exterior Slope

Name: Clay Fill: $\phi=20$, $c=5$
Unit Weight: 19 kN/m^3
Cohesion: 5 kPa
 $\phi: 20^\circ$
Piezometric Line: 1

Name: Insitu Clay: $c = 5$, $\phi = 14$
Unit Weight: 17 kN/m^3
Cohesion: 5 kPa
 $\phi: 14^\circ$
Piezometric Line: 1

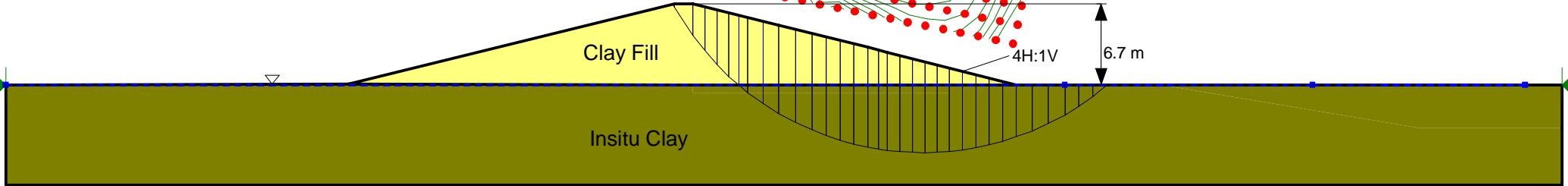


Clay Fill

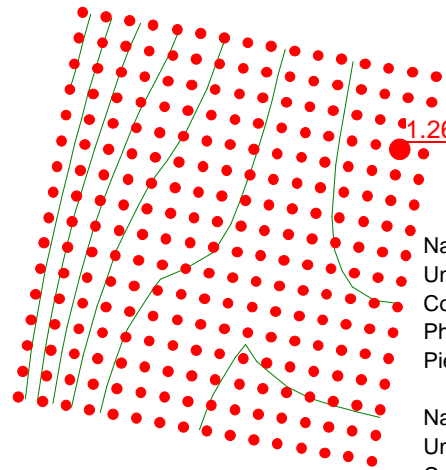
Insitu Clay

4H:1V

6.7 m

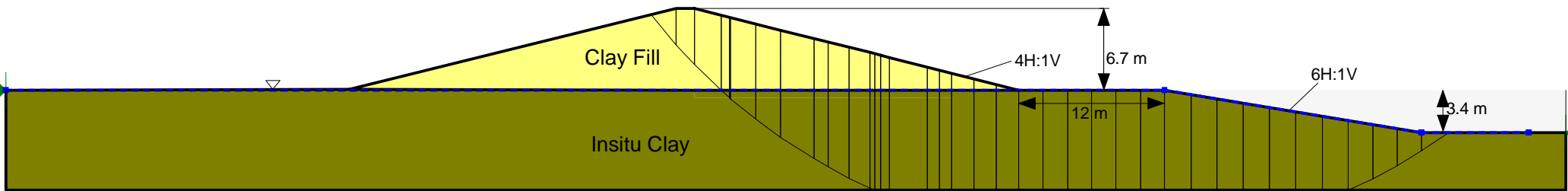


Backstop Berm - 6.7m height
Exterior Slope
Excavation 3.4 m below ground



Name: Clay Fill: $\phi=20$, $c=5$
Unit Weight: 19 kN/m^3
Cohesion: 5 kPa
 $\phi: 20^\circ$
Piezometric Line: 1

Name: Insitu Clay: $c = 5$, $\phi = 14$
Unit Weight: 17 kN/m^3
Cohesion: 5 kPa
 $\phi: 14^\circ$
Piezometric Line: 1



Clay Fill

Insitu Clay

4H:1V

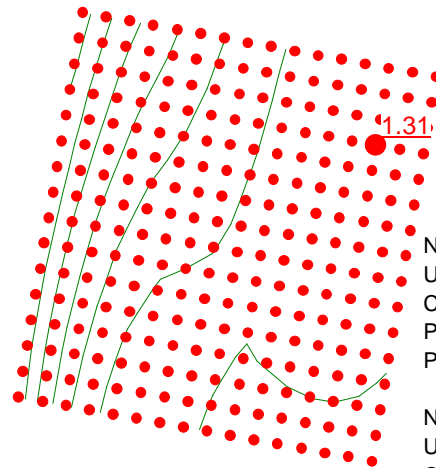
6.7 m

12 m

6H:1V

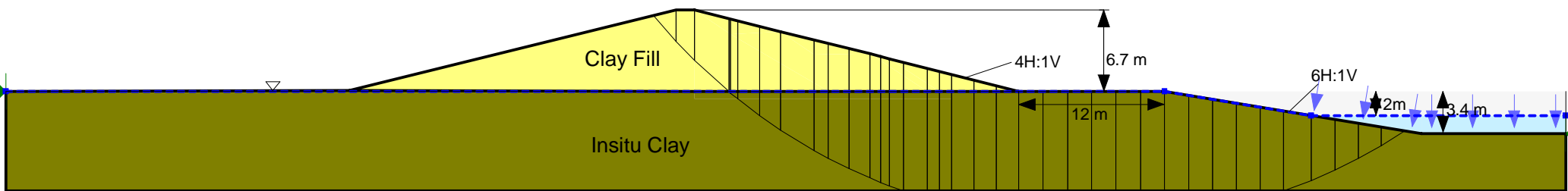
3.4 m

Backstop Berm - 6.7m height
Exterior Slope
Pond level 2 m below grade

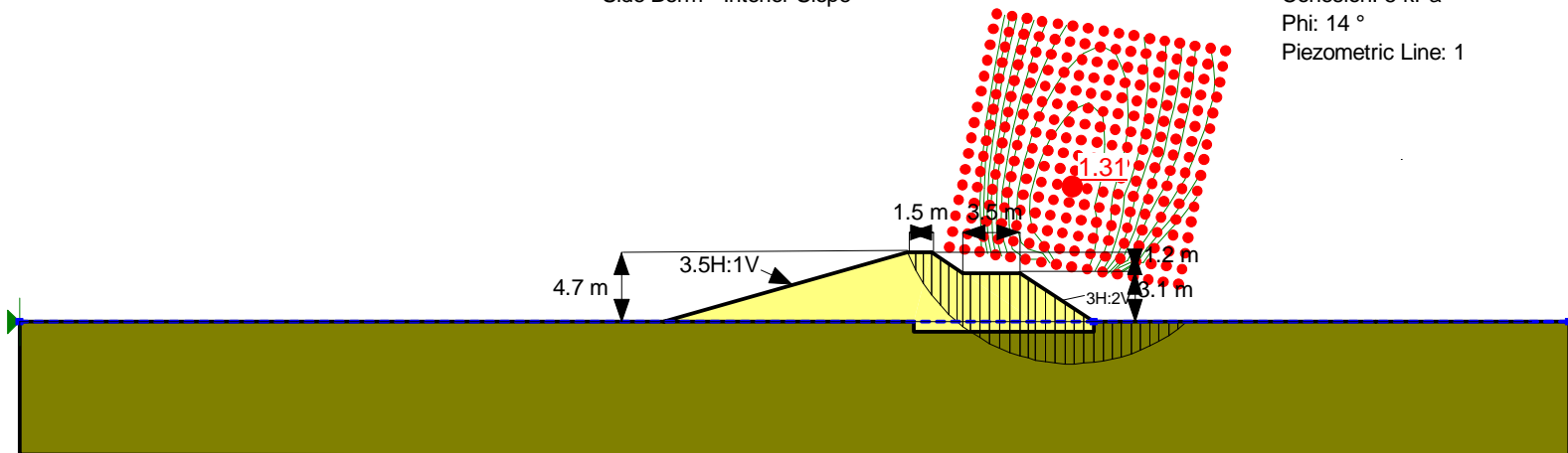


Name: Clay Fill: $\phi=20$, $c=5$
Unit Weight: 19 kN/m^3
Cohesion: 5 kPa
 $\phi: 20^\circ$
Piezometric Line: 1

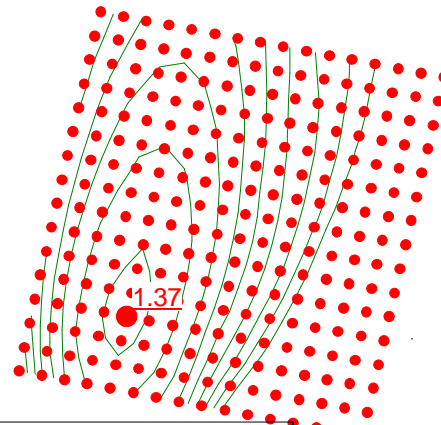
Name: Insitu Clay: $c = 5$, $\phi = 14$
Unit Weight: 17 kN/m^3
Cohesion: 5 kPa
 $\phi: 14^\circ$
Piezometric Line: 1



Side Berm - Interior Slope

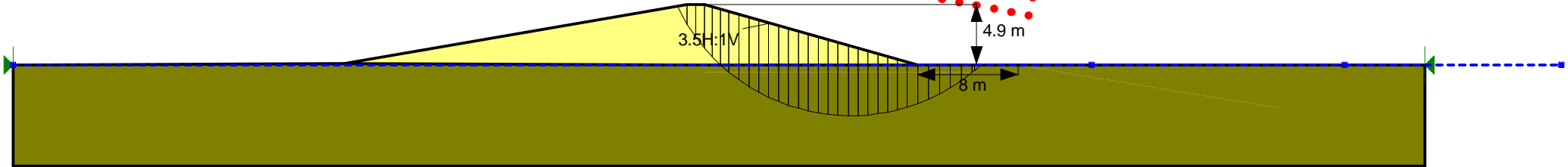


Side Berm
Exterior Slope

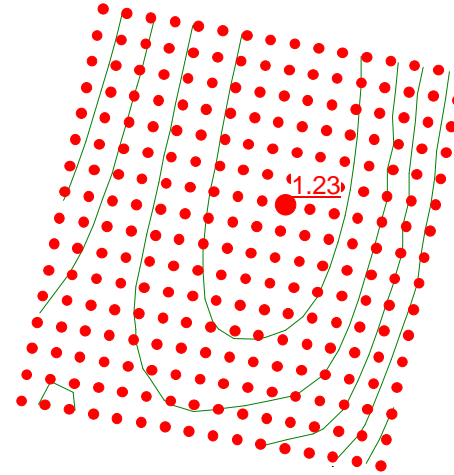


Name: Clay Fill: $\phi=20$, $c=5$
Unit Weight: 19 kN/m^3
Cohesion: 5 kPa
 $\phi: 20^\circ$
Piezometric Line: 1

Name: Insitu Clay: Undrained - $c = 5$, $\phi = 14$
Unit Weight: 17 kN/m^3
Cohesion: 5 kPa
 $\phi: 14^\circ$
Piezometric Line: 1

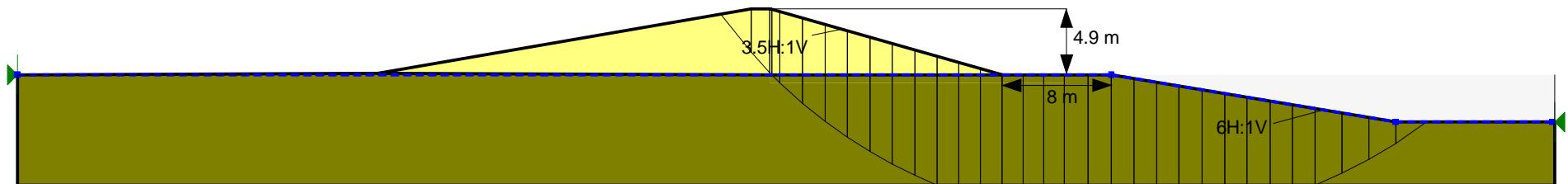


Side Berm
Exterior Slope
Excavation 3.4 m below grade

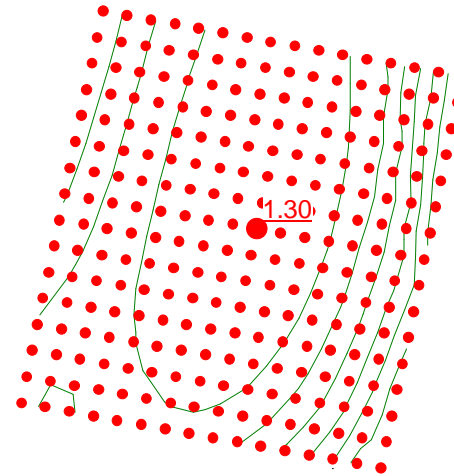


Name: Clay Fill: $\phi=20$, $c=5$
Unit Weight: 19 kN/m^3
Cohesion: 5 kPa
 $\phi: 20^\circ$
Piezometric Line: 1

Name: Insitu Clay: Undrained - $c = 5$, $\phi = 14$
Unit Weight: 17 kN/m^3
Cohesion: 5 kPa
 $\phi: 14^\circ$
Piezometric Line: 1



Side Berm
Exterior Slope
Pond Level 2 m below grade



Name: Clay Fill: $\phi=20$, $c=5$
Unit Weight: 19 kN/m^3
Cohesion: 5 kPa
 $\phi: 20^\circ$
Piezometric Line: 1

Name: Insitu Clay: Undrained - $c = 5$, $\phi = 14$
Unit Weight: 17 kN/m^3
Cohesion: 5 kPa
 $\phi: 14^\circ$
Piezometric Line: 1

